



**Calhoun: The NPS Institutional Archive**  
**DSpace Repository**

---

Theses and Dissertations

1. Thesis and Dissertation Collection, all items

---

1970-04

Investigation of the accuracy of using  
steady-state results to approximate actual  
system availability.

Catron, George Richard

---

<http://hdl.handle.net/10945/15046>

---

*Downloaded from NPS Archive: Calhoun*



Calhoun is the Naval Postgraduate School's public access digital repository for research materials and institutional publications created by the NPS community. Calhoun is named for Professor of Mathematics Guy K. Calhoun, NPS's first appointed -- and published -- scholarly author.

**Dudley Knox Library / Naval Postgraduate School**  
**411 Dyer Road / 1 University Circle**  
**Monterey, California USA 93943**

<http://www.nps.edu/library>

INVESTIGATION OF THE ACCURACY OF USING  
STEADY-STATE RESULTS TO APPROXIMATE  
ACTUAL SYSTEM AVAILABILITY

George Richard Catron



# United States Naval Postgraduate School



## THESIS

INVESTIGATION OF THE ACCURACY OF USING  
STEADY-STATE RESULTS TO APPROXIMATE  
ACTUAL SYSTEM AVAILABILITY

by

George Richard Catron

April 1970

*This document has been approved for public re-  
lease and sale; its distribution is unlimited.*

T133787



Investigation of the Accuracy of Using  
Steady-State Results to Approximate  
Actual System Availability

by

George Richard Catron  
Major, United States Army  
B.S., University of Arizona, 1959

Submitted in partial fulfillment of the  
requirements for the degree of

MASTER OF SCIENCE IN OPERATIONS RESEARCH

from the  
NAVAL POSTGRADUATE SCHOOL  
April 1970

Thesis 0333  
2.1

## ABSTRACT

Values of system availability are computed for a system whose failure density is exponential ( $\lambda$ ) and whose repair density is special Erlang ( $\mu, \alpha$ ). The system is modeled as an alternating renewal process. The Laplace transform of the availability function is developed and inverted (by using a numerical procedure) to obtain the values of the system availability.

Corresponding values of the long-run average system availability and the average availability over the first mission time are also computed. Comparisons are made which establish that using the long-run average value to approximate the true availability over the first mission time is a conservative practice.

# TABLE OF CONTENTS

I.	INTRODUCTION -----	5
	A. THE SYSTEM -----	5
	B. DEFINITION OF AVAILABILITY -----	5
	C. METHOD CURRENTLY PRACTICED TO DETERMINE AVAILABILITY -----	6
	D. OBJECTIVES OF THIS RESEARCH -----	7
II.	SUMMARY AND CONCLUSIONS -----	8
III.	THE MODEL -----	10
	A. DESCRIPTION -----	10
	B. SOLUTION -----	12
	1. Laplace Transforms -----	12
	2. The Inverse Transform -----	13
IV.	DESCRIPTION OF THE COMPUTER PROGRAM -----	15
	APPENDIX A: RESULTS -----	17
	APPENDIX B: EXAMPLE PROBLEM -----	34
	APPENDIX C: FORTRAN IV COMPUTER PROGRAM FOR THE INVERSION OF $\eta^*(s)$ BY NUMERICAL METHODS -----	36
	BIBLIOGRAPHY -----	39
	INITIAL DISTRIBUTION LIST -----	40
	FORM DD 1473 -----	41





## I. INTRODUCTION

### A. THE SYSTEM

Most physical systems people encounter are of the type which operate for a time, fail, are repaired and put back into operation. The system then may be said to have two states. Truly, each of these states may be the union of numerous sub-states, but the two major states prevail.

Some usual terms applied to the first state are 'operational', 'available' or 'up'. This is the state or condition of the system when it is capable of accomplishing the task for which it was designed and built. The second state, the complement of the first, is the less desirable state and is usually termed 'failed', 'nonoperational', 'unavailable' or 'down'.

Hereinafter the system states will be referred to as 'up' or 'down'.

### B. DEFINITION OF AVAILABILITY

A good deal of effort is being expended by the U.S. Government and by private industry to obtain measures of certain quality characteristics applicable to such systems as is described in A. Hosford [2] has discussed several of these characteristics.

One such quality characteristic that is of primary concern is system availability. The 'system availability' or simply 'availability' is the probability that the

system is up at any time  $t \geq 0$ , given it was up at time zero.

The availability function,  $\eta(t)$ , is a real valued function which gives this probability for any time  $t \geq 0$ .

#### C. METHOD CURRENTLY PRACTICED TO DETERMINE AVAILABILITY

In reliability literature, availability is often defined differently as:

$$A = \frac{MTTF}{MTTF + MRT}$$

where MTTF is Mean-Time-To-Failure and MRT is Mean-Repair-Time. This definition provides the only method currently in wide spread use for determining availability.

Note: This quantity has the variable name ZBAR in the computer program and output (Appendices A and C).

Cox [1] has shown that regardless of the distributions of uptimes and downtimes

$$\lim_{t \rightarrow \infty} \eta(t) = A.$$

That is, A is actually the steady-state system availability.

Similarly, it may be shown that the long-run average availability

$$\lim_{t \rightarrow \infty} \frac{1}{t} \int_0^t \eta(x) dx = A.$$

Jacobson [3] describes a statistical procedure for obtaining a confidence interval estimate for A.

#### D. OBJECTIVES OF THIS RESEARCH

The objectives of this research were the following:

1. To compute exact values of the availability function for a system with given distributions of uptimes and downtimes.
2. To compare true availability of a system with that obtained by methods currently in practice.

## II. SUMMARY AND CONCLUSIONS

A physical system having an 'up' state and a 'down' state and with the ability to transit between the two states was modeled as an alternating renewal process for the purpose of finding the system's availability function,  $\eta(t)$ . An explicit general expression for  $\eta(t)$  was not found because of the complex structure of the model equations under the assumed distributions of uptimes and downtimes. However,  $\eta^*(s)$ , the Laplace transform of  $\eta(t)$ , was developed from the assumed probability density functions and the renewal density functions of the model.

A computer program was written to use a numerical procedure to invert the Laplace transform for specific values of the parameters and of time, the independent variable.

Upon consideration of the results and some sample problems (see Appendices A and B) the following conclusions were made.

1. Under the fairly realistic assumptions of the model, exact values of  $\eta(t)$  can be and were computed.
2. Use of long-run average availability to approximate the true availability over the first mission time, as is currently being done in practice, is a conservative procedure.

3. The amount by which the long-run average availability underestimates the true availability during the first mission time is dependent upon the long-run value, i.e., the lower the long-run value, the more it underestimates the true availability.

### III. THE MODEL

#### A. DESCRIPTION

The system was modeled as an alternating renewal process with two states. That is, the new system was assumed to start operating in the up state. The time spent in this state before the first failure, whether in use or just available for use, was a random variable  $U_1$ . Upon failure the system entered the down state. The time spent down before the first repair, whether awaiting repairs or actually being repaired, was a random variable  $D_1$ . The length of the first cycle was the random time  $U_1 + D_1$ .

It was assumed the system kept alternating between up and down and each repair returned it to 'like new' condition so that the uptimes  $U_i, i=1,2,\dots$ , were taken to be independent, identically distributed random variables. They were assumed to be exponentially distributed with parameter  $\lambda > 0$  and probability density function

$$f_U(t) = \begin{cases} 0 & , t < 0 \\ \lambda e^{-\lambda t} & , 0 \leq t \end{cases}.$$

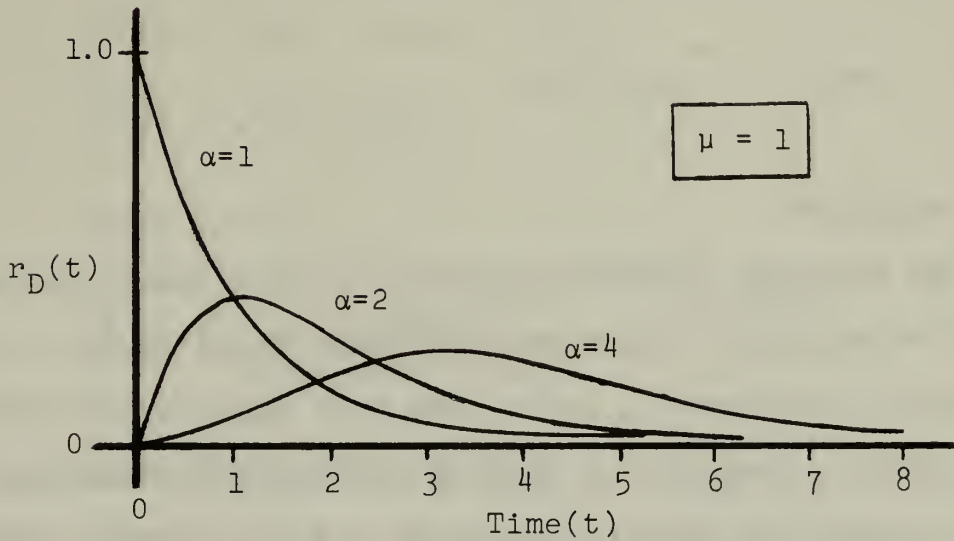
Note: All time units in this thesis are mission times.

The downtimes  $D_i, i=1,2,\dots$ , were also assumed to be independent, identically distributed random variables and independent of the uptimes. They were assumed to have a



special Erlang distribution with parameters  $\mu > 0$  and  $\alpha=1,2,\dots$ , and with probability density function.

$$r_D(t) = \begin{cases} 0 & , \quad t < 0 \\ \frac{\mu^\alpha}{(\alpha-1)!} t^{\alpha-1} e^{-\mu t} & , \quad 0 \leq t \end{cases}$$



The Special Erlang Density Function

Weiss [5], through a simple argument, has shown the renewal density functions for such a renewal process to be

$$W_0(t) = f_U(t) + \int_0^t W_1(\tau) f_U(t-\tau) d\tau$$

$$W_1(t) = \int_0^t W_0(\tau) r_D(t-\tau) d\tau$$



where 0 and 1 are subscripts for 'up' and 'down' respectively and  $W_j(t)$  is the renewal density for the event "end of stay in state j". Weiss has also given the availability function as:

$$\eta(t) = R(t) + \int_0^t W_1(\tau) R(t-\tau) d\tau$$

where  $R(t)$  is the reliability function, i.e.,

$$R(t) = \int_t^\infty f_U(x) dx.$$

## B. SOLUTION

No straight forward solution of these equations for  $\eta(t)$  in explicit closed form has been found except in the special case where  $f_U$  and  $r_D$  are both exponential density functions. However, by finding the Laplace transforms of the probability density functions and the renewal density functions the Laplace transform of the availability function was found.

### 1. Laplace Transforms

The Laplace transform of a continuous or sectionally continuous function  $g(t)$ ,  $t$  in  $[0, \infty)$ , is

$$g^*(s) = \int_0^\infty e^{-st} g(t) dt ; \quad s \text{ is a complex constant}$$

whose real part is large enough that the integral converges.

The Laplace transform of  $f_U(t)$  is

$$\begin{aligned}
 f_U^*(s) &= \int_0^{\infty} e^{-st} f_U(t) dt = \int_0^{\infty} e^{-st} \lambda e^{-\lambda t} dt \\
 &= \frac{\lambda}{\lambda+s} \int_0^{\infty} (\lambda+s) e^{-(\lambda+s)t} dt = \frac{\lambda}{\lambda+s} .
 \end{aligned}$$

Similarly,  $r_D^*(s)$  may be shown to equal  $\left(\frac{\mu}{\mu+s}\right)^\alpha$ .

The Laplace transforms of the renewal densities are:

$$w_0^*(s) = f_U^*(s) + w_1^*(s) f_U^*(s)$$

$$w_1^*(s) = w_0^*(s) r_D^*(s) .$$

These imply

$$w_0^*(s) = \frac{\lambda(\mu+s)^\alpha}{(\lambda+s)(\mu+s)^\alpha - \lambda\mu^\alpha} .$$

Noting that in this case

$$\eta(t) = \frac{w_0(t)}{\lambda} ,$$

the Laplace transform of the availability function was found to be

$$\eta^*(s) = \frac{(\mu+s)^\alpha}{(\lambda+s)(\mu+s)^\alpha - \lambda\mu^\alpha} .$$

## 2. The Inverse Transform

The desired solution for the availability function is the inverse transform of  $\eta^*(s)$ . As before, no method was found to obtain an explicit general expression for  $\eta(t)$ .

Therefore a numerical inversion procedure was used to compute values of  $\eta(t)$  for particular values of the parameters  $\lambda$ ,  $\mu$ , and  $\alpha$  and for values of  $t=.05$ ,  $.10$ ,  $.15$ , ...,  $1.0$  mission times.

Several values were chosen for the parameters  $\lambda$ ,  $\mu$  and  $\alpha$  over a range that was judged to be of practical interest. Those values and the corresponding values of  $\eta(t)$  are shown in Appendix A.

#### IV. DESCRIPTION OF THE COMPUTER PROGRAM

The computations were done by a computer program written in FORTRAN IV programming language and run on the IBM system/360, model 67 computer at the Naval Postgraduate School (see program listing, Appendix C). The program listing contains enough explanatory comments to enable the reader familiar with FORTRAN to follow the procedure.

The following are the major steps:

1. The polynomial in the denominator of  $\eta^*(s)$  was expanded to the form  $a_0 + a_1s + a_2s^2 + \dots + s^{\alpha+1}$ . That is,

$$(\lambda+s)(\mu+s)^\alpha - \lambda\mu^\alpha = \sum_{j=1}^{\alpha} \binom{\alpha}{j} \mu^{\alpha-j} \left(\lambda + \frac{j\mu}{\alpha+1-j}\right) s^j + s^{\alpha+1}.$$

Note that  $a_0$  equals zero.

2. A computer library subroutine which employs the Newton-Raphson successive approximations technique was used to find the roots of this polynomial.

3. After the roots were checked to see that they were all different the following formula was used in computing the values of  $\eta(t)$ . Often called Heaviside's expansion formula [4] it is an application of the residue theorem from theory of complex variables.

Heaviside's Expansion Formula: let  $P(s)$  and  $Q(s)$  be polynomials where  $P(s)$  has degree less than that of  $Q(s)$ . If  $Q(s)$  has distinct roots  $A_k$ ,  $k=1,2,\dots,n$ , then the inverse Laplace transform of  $\frac{P(s)}{Q(s)}$  is

$$L^{-1} \left( \frac{P(s)}{Q(s)} \right) = \sum_{k=1}^n \frac{P(A_k)}{Q'(A_k)} e^{A_k t}.$$

By application of this formula

$$L^{-1}(\eta^*(s)) = \eta(t) = \sum_{k=1}^{\alpha+1} \frac{\mu + A_k}{\mu + A_k + \alpha(\lambda + A_k)} e^{A_k t}.$$

## APPENDIX A

### RESULTS

This appendix contains tabulated values of the availability function for the indicated sets of parameters and the indicated time in mission-time units.

The values of PZERO given are such that PZERO equals the probability of a repair in less than one mission time, i.e.,

$$\int_0^1 \frac{\mu^\alpha}{(\alpha-1)!} t^{\alpha-1} e^{-\mu t} dt = \text{PZERO} .$$

Z1 is the average availability over the first mission time.

$$Z1 = \frac{1}{20} \left( \frac{\eta(0)+\eta(1)}{2} + \sum_{i=1}^{19} \eta(.05i) \right)$$

ZBAR is the asymptotic value of  $\eta(t)$  for large  $t$ . ZBAR is also the long-run average availability.

$$ZBAR = \frac{MTTF}{MTTF + MTR} = \frac{1/\lambda}{1/\lambda + \alpha/\mu} = \frac{\mu}{\mu + \alpha\lambda}$$

Example: For a system whose uptimes have the exponential ( $\lambda = .005$ ) distribution and whose downtimes have the Erlang ( $\mu = 2.03$ ,  $\alpha = 2$ ) distribution, the true system availability at a half mission time is  $\eta(.5) = .99777$ .

The true average availability over the first mission time is  $Z_1 = .99792$  and the long-run average availability is  $Z_{BAR} = .99510$ .



ALPHA= 2.0

PZERO= 0.60

MU= 2.03

TIME	LAMBDA						
	.005	.010	.050	.100	.200	.300	.400
0.05	.99975	.99950	.99751	.99502	.99007	.98514	.98023
0.10	.99950	.99901	.99504	.99011	.98032	.97063	.96103
0.15	.99926	.99852	.99263	.98531	.97084	.95658	.94254
0.20	.99902	.99805	.99027	.98064	.96167	.94307	.92484
0.25	.99879	.99759	.98799	.97614	.95286	.93016	.90802
0.30	.99857	.99714	.98580	.97180	.94444	.91788	.89210
0.35	.99836	.99671	.98369	.96766	.93642	.90626	.87712
0.40	.99815	.99631	.98167	.96370	.92982	.89530	.86308
0.45	.99795	.99591	.97975	.95995	.92164	.88501	.84997
0.50	.99777	.99554	.97793	.95639	.91489	.87538	.83778
0.55	.99759	.99519	.97620	.95303	.90854	.86640	.82647
0.60	.99742	.99485	.97456	.94987	.90260	.85804	.81602
0.65	.99726	.99454	.97302	.94689	.89706	.85029	.80639
0.70	.99711	.99424	.97157	.94410	.89189	.84312	.79754
0.75	.99697	.99396	.97021	.94149	.88709	.83650	.78943
0.80	.99684	.99369	.96894	.93905	.88264	.83040	.78201
0.85	.99671	.99344	.96774	.93678	.87851	.82470	.77524
0.90	.99660	.99321	.96663	.93466	.87470	.81965	.76908
0.95	.99649	.99299	.96559	.93270	.87119	.81494	.76349
1.00	.99639	.99279	.96462	.93087	.86795	.81064	.75842
Z1	.99792	.99584	.97945	.95954	.92151	.88574	.85208
ZBAR	.99510	.99024	.95305	.91031	.83539	.77186	.71731



ALPHA= 2.0

PZERO= 0.70

MU= 2.45

	LAMBDA						
TIME	.005	.010	.050	.100	.200	.300	.400
0.05	.99975	.99950	.99751	.99502	.99007	.98515	.98025
0.10	.99950	.99901	.99506	.99014	.98037	.97071	.96114
0.15	.99926	.99853	.99267	.98539	.97100	.95682	.94286
0.20	.99903	.99806	.99036	.98082	.96202	.94360	.92553
0.25	.99881	.99762	.98815	.97646	.95349	.93109	.90925
0.30	.99860	.99719	.98605	.97231	.94544	.91935	.89404
0.35	.99839	.99679	.98406	.96840	.93788	.90840	.87992
0.40	.99820	.99641	.98219	.96472	.93081	.89822	.86689
0.45	.99802	.99605	.98043	.96128	.92424	.88881	.85492
0.50	.99785	.99571	.97878	.95807	.91816	.88016	.84397
0.55	.99770	.99540	.97725	.95510	.91254	.87222	.83400
0.60	.99755	.99511	.97582	.95234	.90738	.86497	.82495
0.65	.99741	.99484	.97450	.94979	.90264	.85836	.81676
0.70	.99729	.99458	.97328	.94745	.89831	.85236	.80938
0.75	.99717	.99435	.97216	.94529	.89436	.84693	.80275
0.80	.99706	.99414	.97112	.94331	.89076	.84203	.79681
0.85	.99696	.99394	.97017	.94151	.88750	.83761	.79150
0.90	.99687	.99376	.96930	.93985	.88454	.83364	.78678
0.95	.99679	.99359	.96850	.93835	.88186	.83008	.78257
1.00	.99671	.99343	.96777	.93698	.87945	.82689	.77885
Z1	.99803	.99606	.98056	.96170	.92566	.89170	.85968
ZBAR	.99593	.99190	.96078	.92453	.85965	.80328	.75385

ALPHA= 2.0

PZERO= 0.80

MU= 3.00

TIME	LAMBDA						
	.005	.010	.050	.100	.200	.300	.400
0.05	.99975	.99950	.99751	.99503	.99008	.98516	.98027
0.10	.99951	.99901	.99508	.99018	.98045	.97083	.96130
0.15	.99927	.99854	.99273	.98552	.97125	.95719	.94334
0.20	.99905	.99809	.99050	.98109	.96255	.94437	.92656
0.25	.99883	.99767	.98839	.97692	.95441	.93245	.91103
0.30	.99863	.99727	.98642	.97304	.94687	.92146	.89630
0.35	.99845	.99690	.98459	.96944	.93992	.91141	.88386
0.40	.99827	.99655	.98290	.96613	.93357	.90226	.87216
0.45	.99812	.99624	.98135	.96310	.92779	.89400	.86166
0.50	.99797	.99595	.97993	.96034	.92256	.88657	.85227
0.55	.99784	.99568	.97863	.95783	.91784	.87991	.84393
0.60	.99772	.99544	.97746	.95556	.91360	.87398	.83655
0.65	.99761	.99522	.97640	.95352	.90981	.86871	.83004
0.70	.99751	.99502	.97544	.95168	.90643	.86404	.82433
0.75	.99742	.99484	.97458	.95003	.90342	.85993	.81933
0.80	.99734	.99468	.97381	.94856	.90076	.85632	.81498
0.85	.99726	.99454	.97311	.94724	.89840	.85315	.81120
0.90	.99720	.99441	.97249	.94607	.89632	.85037	.80792
0.95	.99714	.99429	.97194	.94503	.89449	.84796	.80509
1.00	.99709	.99419	.97145	.94411	.89288	.84586	.80266
Z1	.99817	.99635	.98195	.96442	.93085	.89915	.86920
ZBAR	.99668	.99338	.96774	.93750	.88235	.83333	.78947

ALPHA= 2.0

PZERO= 0.90

MU= 3.90

TIME	LAMBDA						
	.005	.010	.050	.100	.200	.300	.400
0.05	.99975	.99950	.99752	.99504	.99011	.98520	.98031
0.10	.99951	.99902	.99512	.99026	.98061	.97106	.96151
0.15	.99928	.99857	.99285	.98575	.97171	.95788	.94426
0.20	.99907	.99814	.99074	.98158	.96352	.94582	.92846
0.25	.99888	.99775	.98881	.97777	.95608	.93492	.91428
0.30	.99870	.99740	.98707	.97433	.94940	.92520	.90170
0.35	.99854	.99708	.98550	.97125	.94346	.91661	.89066
0.40	.99840	.99680	.98410	.96851	.93823	.90909	.88106
0.45	.99827	.99654	.98287	.96610	.93364	.90255	.87276
0.50	.99816	.99632	.98178	.96399	.92965	.89689	.86565
0.55	.99806	.99613	.98083	.96215	.92619	.89204	.85958
0.60	.99797	.99595	.98000	.96054	.92321	.88789	.85444
0.65	.99790	.99581	.97928	.95916	.92066	.88435	.85011
0.70	.99783	.99568	.97865	.95796	.91847	.88136	.84647
0.75	.99778	.99556	.97811	.95694	.91661	.87884	.84343
0.80	.99773	.99547	.97765	.95605	.91503	.87672	.84090
0.85	.99769	.99538	.97725	.95530	.91370	.87494	.83891
0.90	.99765	.99531	.97691	.95466	.91257	.87346	.83708
0.95	.99762	.99525	.97662	.95412	.91162	.87223	.83566
1.00	.99759	.99520	.97637	.95365	.91083	.87121	.83450
Z1	.99838	.99676	.98399	.96841	.93850	.91013	.88323
ZBAR	.99744	.99490	.97500	.95122	.90698	.86667	.82979

ALPHA= 2.0

PZERO= 0.95

MU= 4.80

LAMBDA

TIME	.005	.010	.050	.100	.200	.300	.400
0.05	.99975	.99950	.99752	.99505	.99013	.98524	.98037
0.10	.99952	.99903	.99516	.99035	.98080	.97134	.96198
0.15	.99930	.99859	.99298	.98602	.97225	.95868	.94531
0.20	.99910	.99820	.99102	.98212	.96460	.94741	.93057
0.25	.99892	.99784	.98927	.97868	.95787	.93757	.91776
0.30	.99877	.99753	.98775	.97567	.95204	.92910	.90681
0.35	.99863	.99727	.98643	.97308	.94705	.92189	.89755
0.40	.99852	.99704	.98529	.97086	.94282	.91581	.88981
0.45	.99842	.99684	.98433	.96899	.93925	.91074	.88340
0.50	.99833	.99667	.98352	.96741	.93628	.90654	.87813
0.55	.99826	.99653	.98283	.96608	.93381	.90308	.87383
0.60	.99820	.99641	.98226	.96498	.93177	.90025	.87035
0.65	.99815	.99631	.98178	.96407	.93009	.89795	.86754
0.70	.99811	.99623	.98138	.96331	.92872	.89609	.86529
0.75	.99808	.99616	.98106	.96269	.92760	.89458	.86349
0.80	.99805	.99611	.98079	.96218	.92669	.89338	.86207
0.85	.99803	.99606	.98056	.96176	.92596	.89242	.86095
0.90	.99801	.99602	.98038	.96142	.92537	.89165	.86007
0.95	.99799	.99599	.98023	.96114	.92490	.89104	.85938
1.00	.99798	.99596	.98011	.96092	.92452	.89056	.85885
Z1	.99856	.99712	.98573	.97182	.94501	.91950	.89521
ZBAR	.99792	.99585	.97959	.96000	.92308	.88889	.85714



ALPHA= 3.0

PZERO= 0.60

MU= 3.11

TIME	LAMBDA						
	.005	.010	.050	.100	.200	.300	.400
0.05	.99975	.99950	.99750	.99501	.99005	.98511	.98020
0.10	.99950	.99900	.99502	.99006	.98022	.97048	.96083
0.15	.99925	.99851	.99255	.98516	.97054	.95614	.94195
0.20	.99901	.99802	.99012	.98034	.96106	.94217	.92365
0.25	.99877	.99753	.98773	.97562	.95184	.92865	.90603
0.30	.99853	.99706	.98541	.97103	.94291	.91563	.88916
0.35	.99830	.99661	.98315	.96659	.93434	.90320	.87313
0.40	.99808	.99616	.98098	.96233	.92615	.89138	.85799
0.45	.99787	.99574	.97889	.95826	.91837	.88023	.84379
0.50	.99766	.99534	.97691	.95439	.91102	.86978	.83055
0.55	.99747	.99495	.97503	.95074	.90413	.86002	.81828
0.60	.99729	.99459	.97325	.94730	.89768	.85097	.80698
0.65	.99712	.99424	.97158	.94408	.89170	.84262	.79664
0.70	.99695	.99392	.97002	.94108	.88616	.83495	.78721
0.75	.99680	.99362	.96857	.93830	.88106	.82795	.77868
0.80	.99666	.99334	.96722	.93572	.87638	.82159	.77099
0.85	.99653	.99308	.96597	.93334	.87210	.81583	.76410
0.90	.99641	.99284	.96481	.93116	.86822	.81064	.75796
0.95	.99630	.99261	.96375	.92917	.86469	.80599	.75251
1.00	.99619	.99241	.96278	.92735	.86151	.80183	.74770
Z1	.99782	.99564	.97849	.95767	.91797	.88071	.84572
ZBAR	.99520	.99045	.95399	.91202	.83827	.77556	.72158

ALPHA= 3.0

PZERO= 0.70

MU= 3.62

TIME	LAMBDA						
	.005	.010	.050	.100	.200	.300	.400
0.05	.99975	.99950	.99750	.99501	.99005	.98512	.98020
0.10	.99950	.99900	.99502	.99007	.98023	.97049	.96085
0.15	.99925	.99851	.99255	.98518	.97059	.95621	.94205
0.20	.99901	.99802	.99015	.98040	.96120	.94237	.92392
0.25	.99877	.99755	.98780	.97576	.95212	.92907	.90659
0.30	.99854	.99709	.98554	.97129	.94343	.91640	.89016
0.35	.99832	.99665	.98336	.96702	.93517	.90443	.87474
0.40	.99811	.99623	.98130	.96296	.92739	.89321	.86038
0.45	.99791	.99583	.97934	.95915	.92011	.88279	.84713
0.50	.99773	.99546	.97751	.95559	.91335	.87318	.83498
0.55	.99755	.99511	.97581	.95227	.90711	.86438	.82394
0.60	.99739	.99478	.97422	.94921	.90140	.85637	.81397
0.65	.99724	.99448	.97277	.94640	.89619	.84913	.80503
0.70	.99710	.99420	.97143	.94384	.89147	.84263	.79708
0.75	.99697	.99395	.97020	.94150	.88721	.83682	.79004
0.80	.99685	.99372	.96909	.93939	.88340	.83167	.78386
0.85	.99675	.99351	.96808	.93748	.87999	.82711	.77846
0.90	.99665	.99332	.96717	.93577	.87696	.82311	.77377
0.95	.99656	.99314	.96635	.93423	.87429	.81962	.76973
1.00	.99649	.99299	.96562	.93287	.87193	.81658	.76627
71	.99791	.99583	.97940	.95945	.92138	.88562	.85200
7BAR	.99587	.99178	.96021	.92347	.85782	.80088	.75104

ALPHA= 3.0

PZERO= 0.80

MU= 4.30

TIME	LAMBDA						
	.005	.010	.050	.100	.200	.300	.400
0.05	.99975	.99950	.99750	.99501	.99005	.98512	.98021
0.10	.99950	.99900	.99503	.99008	.98025	.97052	.96089
0.15	.99926	.99851	.99259	.98523	.97067	.95634	.94221
0.20	.99902	.99803	.99021	.98052	.96142	.94270	.92436
0.25	.99879	.99757	.98792	.97600	.95259	.92976	.90750
0.30	.99857	.99713	.98575	.97171	.94426	.91762	.89177
0.35	.99836	.99672	.98370	.96768	.93648	.90636	.87728
0.40	.99816	.99633	.98179	.96394	.92930	.89603	.86407
0.45	.99798	.99597	.98002	.96049	.92274	.88665	.85215
0.50	.99782	.99564	.97841	.95735	.91678	.87820	.84151
0.55	.99766	.99534	.97694	.95450	.91143	.87068	.83210
0.60	.99753	.99506	.97561	.95193	.90666	.86402	.82385
0.65	.99740	.99482	.97441	.94964	.90243	.85818	.81668
0.70	.99729	.99460	.97335	.94760	.89872	.85309	.81050
0.75	.99719	.99440	.97240	.94581	.89547	.84869	.80522
0.80	.99711	.99422	.97157	.94423	.89264	.84491	.80074
0.85	.99703	.99407	.97083	.94284	.89020	.84169	.79697
0.90	.99696	.99393	.97019	.94164	.88810	.83896	.79383
0.95	.99690	.99381	.96963	.94060	.88631	.83666	.79122
1.00	.99685	.99371	.96914	.93970	.88479	.83474	.78908
Z1	.99803	.99608	.98062	.96183	.92595	.89218	.86038
ZBAR	.99652	.99307	.96629	.93478	.87755	.82692	.78182

ALPHA= 3.0

PZERO= 0.90

MU= 5.35

LAMBDA

TIME	.005	.010	.050	.100	.200	.300	.400
0.05	.99975	.99950	.99750	.99502	.99006	.98512	.98021
0.10	.99950	.99901	.99504	.99010	.98029	.97058	.96097
0.15	.99926	.99852	.99263	.98531	.97084	.95659	.94255
0.20	.99903	.99806	.99032	.98074	.96187	.94337	.92524
0.25	.99881	.99762	.98815	.97646	.95349	.93110	.90927
0.30	.99861	.99721	.98614	.97250	.94581	.91992	.89479
0.35	.99842	.99684	.98431	.96890	.93887	.90988	.88189
0.40	.99825	.99650	.98266	.96566	.93268	.90100	.87055
0.45	.99810	.99620	.98119	.96280	.92724	.89324	.86074
0.50	.99797	.99594	.97990	.96029	.92251	.88656	.85236
0.55	.99785	.99571	.97877	.95810	.91843	.88087	.84528
0.60	.99775	.99551	.97779	.95623	.91496	.87606	.83938
0.65	.99766	.99533	.97695	.95462	.91203	.87205	.83450
0.70	.99759	.99518	.97623	.95326	.90957	.86873	.83052
0.75	.99752	.99506	.97563	.95211	.90753	.86601	.82731
0.80	.99747	.99495	.97512	.95115	.90585	.86379	.82474
0.85	.99742	.99486	.97469	.95036	.90447	.86201	.82271
0.90	.99739	.99478	.97433	.94970	.90334	.86059	.82112
0.95	.99735	.99472	.97403	.94915	.90244	.85947	.81990
1.00	.99733	.99466	.97379	.94871	.90171	.85858	.81896
Z1	.99822	.99644	.98241	.96534	.93266	.90181	.87268
ZBAR	.99720	.99442	.97273	.94690	.89916	.85600	.81679



ALPHA= 3.0

PZERO= 0.95

MU= 6.30

TIME	LAMBDA						
	.005	.010	.050	.100	.200	.300	.400
0.05	.99975	.99950	.99751	.99502	.99006	.98513	.98022
0.10	.99950	.99901	.99505	.99012	.98034	.97066	.96107
0.15	.99927	.99853	.99268	.98541	.97105	.95689	.94295
0.20	.99904	.99808	.99045	.98100	.96238	.94413	.92624
0.25	.99883	.99767	.98841	.97696	.95448	.93257	.91119
0.30	.99865	.99730	.98656	.97333	.94744	.92233	.89796
0.35	.99848	.99697	.98493	.97013	.94129	.91345	.88656
0.40	.99834	.99668	.98352	.96736	.93600	.90587	.87692
0.45	.99821	.99643	.98230	.96500	.93153	.89952	.86891
0.50	.99811	.99622	.98127	.96300	.92779	.89426	.86235
0.55	.99802	.99604	.98041	.96134	.92470	.88997	.85705
0.60	.99794	.99589	.97969	.95997	.92219	.88652	.85284
0.65	.99788	.99577	.97910	.95884	.92015	.88377	.84954
0.70	.99783	.99567	.97862	.95793	.91853	.88160	.84698
0.75	.99779	.99559	.97823	.95720	.91724	.87991	.84502
0.80	.99776	.99552	.97792	.95661	.91623	.87861	.84354
0.85	.99773	.99547	.97766	.95615	.91544	.87762	.84245
0.90	.99771	.99542	.97746	.95578	.91484	.87688	.84164
0.95	.99769	.99539	.97730	.95549	.91437	.87632	.84106
1.00	.99768	.99536	.97718	.95527	.91402	.87591	.84065
Z1	.99837	.99674	.98388	.96821	.93815	.90970	.88274
ZBAR	.99762	.99526	.97674	.95455	.91304	.87500	.84000

ALPHA= 4.0

PZERO= 0.60

MU= 4.20

LAMBDA

TIME	.005	.010	.050	.100	.200	.300	.400
0.05	.99975	.99950	.99750	.99501	.99005	.98511	.98020
0.10	.99950	.99900	.99501	.99005	.98020	.97045	.96080
0.15	.99925	.99850	.99253	.98512	.97047	.95604	.94182
0.20	.99900	.99801	.99007	.98025	.96088	.94191	.92330
0.25	.99876	.99752	.98764	.97544	.95148	.92812	.90533
0.30	.99852	.99703	.98525	.97072	.94231	.91474	.88799
0.35	.99828	.99656	.98292	.96613	.93343	.90185	.87137
0.40	.99805	.99610	.98065	.96168	.92488	.88952	.85556
0.45	.99782	.99565	.97847	.95741	.91671	.87781	.84064
0.50	.99761	.99523	.97637	.95334	.90897	.86678	.82667
0.55	.99741	.99482	.97439	.94948	.90168	.85647	.81371
0.60	.99721	.99444	.97251	.94584	.89488	.84691	.80177
0.65	.99703	.99407	.97075	.94245	.88856	.83811	.79087
0.70	.99686	.99373	.96911	.93929	.88274	.83007	.78101
0.75	.99670	.99342	.96758	.93638	.87742	.82278	.77214
0.80	.99656	.99313	.96618	.93370	.87258	.81622	.76425
0.85	.99642	.99286	.96489	.93126	.86821	.81036	.75727
0.90	.99630	.99261	.96371	.92905	.86428	.80515	.75117
0.95	.99618	.99238	.96264	.92704	.86078	.80057	.74586
1.00	.99608	.99218	.96168	.92524	.85767	.79657	.74130
71	.99776	.99553	.97795	.95661	.91597	.87786	.84212
ZBAR	.99526	.99057	.95455	.91304	.84000	.77778	.72414

ALPHA= 4.0

PZERO= 0.70

MU= 4.76

TIME	LAMBDA						
	.005	.010	.050	.100	.200	.300	.400
0.05	.99975	.99950	.99750	.99501	.99005	.98511	.98020
0.10	.99950	.99900	.99501	.99005	.98020	.97045	.96080
0.15	.99925	.99850	.99254	.98513	.97049	.95606	.94184
0.20	.99900	.99801	.99009	.98027	.96093	.94198	.92340
0.25	.99876	.99752	.98767	.97550	.95161	.92831	.90558
0.30	.99852	.99705	.98532	.97086	.94258	.91513	.88851
0.35	.99829	.99658	.98304	.96637	.93390	.90256	.87229
0.40	.99807	.99614	.98085	.96208	.92565	.89066	.85705
0.45	.99785	.99571	.97876	.95800	.91787	.87952	.84287
0.50	.99765	.99531	.97680	.95418	.91061	.86919	.82982
0.55	.99746	.99494	.97496	.95061	.90389	.85971	.81791
0.60	.99729	.99459	.97325	.94731	.89773	.85108	.80718
0.65	.99713	.99426	.97168	.94429	.89213	.84330	.79759
0.70	.99698	.99396	.97025	.94153	.88708	.83636	.78911
0.75	.99684	.99369	.96894	.93904	.88256	.83021	.78169
0.80	.99672	.99345	.96776	.93681	.87855	.82481	.77526
0.85	.99661	.99323	.96671	.93482	.87501	.82012	.76974
0.90	.99651	.99303	.96576	.93305	.87192	.81608	.76506
0.95	.99642	.99285	.96493	.93150	.86924	.81263	.76113
1.00	.99634	.99269	.96419	.93013	.86692	.80970	.75787
Z1	.99784	.99568	.97870	.95807	.91877	.88191	.84730
ZBAR	.99582	.99167	.95968	.92248	.85612	.79866	.74843

ALPHA= 4.0

P7ERD= 0.80

MU= 5.52

## LAMBDA

TIME	.005	.010	.050	.100	.200	.300	.400
0.05	.99975	.99950	.99750	.99501	.99005	.98511	.98020
0.10	.99950	.99900	.99502	.99006	.98021	.97046	.96081
0.15	.99925	.99850	.99255	.98515	.97051	.95610	.94190
0.20	.99901	.99801	.99011	.98032	.96103	.94212	.92359
0.25	.99877	.99753	.98773	.97562	.95184	.92865	.90603
0.30	.99853	.99707	.98544	.97109	.94304	.91582	.88941
0.35	.99831	.99663	.98324	.96678	.93471	.90376	.87387
0.40	.99810	.99620	.98118	.96273	.92694	.89256	.85954
0.45	.99790	.99581	.97925	.95897	.91976	.88229	.84650
0.50	.99772	.99545	.97747	.95551	.91321	.87300	.83478
0.55	.99755	.99512	.97585	.95236	.90731	.86470	.82440
0.60	.99740	.99481	.97438	.94953	.90205	.85736	.81532
0.65	.99727	.99454	.97307	.94701	.89740	.85096	.80748
0.70	.99714	.99430	.97190	.94478	.89334	.84543	.80078
0.75	.99704	.99409	.97087	.94283	.88983	.84070	.79515
0.80	.99694	.99390	.96997	.94113	.88682	.83671	.79046
0.85	.99686	.99372	.96919	.93967	.88427	.83338	.78661
0.90	.99679	.99359	.96852	.93842	.88212	.83062	.78350
0.95	.99673	.99347	.96794	.93735	.88032	.82837	.78102
1.00	.99667	.99336	.96745	.93645	.87884	.82656	.77908
Z1	.99795	.99590	.97974	.96013	.92271	.88757	.85454
ZBAR	.99639	.99281	.96503	.93243	.87342	.82143	.77528



ALPHA= 4.0

PZERO= 0.90

MU= 6.70

TIME	LAMBDA						
	.005	.010	.050	.100	.200	.300	.400
0.05	.99975	.99950	.99750	.99501	.99005	.98511	.98020
0.10	.99950	.99900	.99502	.99006	.98022	.97048	.96083
0.15	.99925	.99851	.99256	.98518	.97058	.95619	.94202
0.20	.99901	.99802	.99016	.98042	.96124	.94243	.92400
0.25	.99878	.99756	.98786	.97587	.95233	.92938	.90700
0.30	.99856	.99712	.98568	.97157	.94400	.91724	.89128
0.35	.99835	.99671	.98366	.96760	.93633	.90615	.87701
0.40	.99816	.99633	.98181	.96399	.92940	.89620	.86430
0.45	.99799	.99599	.98015	.96075	.92325	.88743	.85320
0.50	.99784	.99569	.97868	.95789	.91787	.87983	.84367
0.55	.99771	.99543	.97739	.95541	.91323	.87335	.83563
0.60	.99760	.99520	.97628	.95327	.90930	.86791	.82896
0.65	.99750	.99500	.97533	.95146	.90599	.86341	.82353
0.70	.99741	.99483	.97453	.94993	.90326	.85975	.81917
0.75	.99734	.99469	.97385	.94867	.90103	.85680	.81574
0.80	.99728	.99457	.97329	.94763	.89922	.85448	.81308
0.85	.99723	.99448	.97283	.94678	.89778	.85266	.81107
0.90	.99719	.99440	.97246	.94609	.89665	.85127	.80958
0.95	.99716	.99433	.97215	.94554	.89576	.85022	.80850
1.00	.99713	.99428	.97191	.94510	.89508	.84944	.80775
Z1	.99811	.99623	.98136	.96328	.92875	.89625	.86563
ZBAR	.99702	.99407	.97101	.94366	.89333	.84810	.80723

ALPHA= 4.0

PZERO= 0.95

MU= 7.80

TIME	LAMBDA						
	.005	.010	.050	.100	.200	.300	.400
0.05	.99975	.99950	.99750	.99501	.99005	.98511	.98020
0.10	.99950	.99900	.99502	.99007	.98024	.97050	.96086
0.15	.99926	.99851	.99258	.98522	.97066	.95632	.94219
0.20	.99902	.99804	.99023	.98056	.96150	.94283	.92453
0.25	.99879	.99759	.98801	.97618	.95294	.93029	.90820
0.30	.99859	.99718	.98597	.97215	.94513	.91892	.89350
0.35	.99840	.99680	.98413	.96854	.93817	.90887	.88058
0.40	.99823	.99647	.98251	.96537	.93211	.90018	.86952
0.45	.99809	.99619	.98110	.96263	.92694	.89283	.86025
0.50	.99797	.99594	.97991	.96032	.92260	.88675	.85267
0.55	.99786	.99573	.97891	.95840	.91904	.88181	.84659
0.60	.99778	.99556	.97808	.95682	.91616	.87788	.84182
0.65	.99771	.99542	.97741	.95554	.91387	.87480	.83816
0.70	.99765	.99531	.97687	.95452	.91207	.87244	.83541
0.75	.99760	.99522	.97644	.95372	.91069	.87065	.83339
0.80	.99757	.99515	.97610	.95309	.90963	.86934	.83195
0.85	.99754	.99509	.97583	.95261	.90884	.86838	.83095
0.90	.99752	.99504	.97563	.95224	.90826	.86771	.83028
0.95	.99750	.99501	.97547	.95196	.90783	.86724	.82985
1.00	.99749	.99498	.97535	.95175	.90753	.86693	.82960
Z1	.99825	.99651	.98277	.96604	.93403	.90382	.87528
ZBAR	.99744	.99490	.97500	.95122	.90698	.86657	.82979

## APPENDIX B

### EXAMPLE PROBLEM

Suppose a system consisting of 15 components is connected in series. Each component, operating independently of the others, has an exponential failure density with parameter  $\lambda$  and a special Erlang repair density with parameters  $\mu$  and  $\alpha$ . Assume that uptimes and downtimes are all independent.

a. What is the average availability of the system over the first mission time if;

(1)  $\lambda = .005$  failures per mission time,  $\mu = 4.8$  repairs per mission time, and  $\alpha = 2$ ?

(2)  $\lambda = .40$  failures per mission time,  $\mu = 4.2$  repairs per mission time, and  $\alpha = 4$ ?

b. What is the long-run average availability of the system if;

(1) the parameters are the same as in a(1)?

(2) the parameters are the same as in a(2)?

Solution:

a.

(1) The average availability of a single component over the first mission time is  $Z_1 = .99856$  (from Appendix A). Letting  $\eta_s$  be the average system availability over the first mission time;

$$\eta_s = (Z_1)^{15} = (.99856)^{15} \doteq \underline{\underline{.9786}}.$$

(2) In this case  $Z1 = .84212$  and  $\eta_s = (.84212)^{15} \doteq \underline{\underline{.0760}}$ .

b.

(1) The long-run average availability of a single component is  $ZBAR = .99792$ .

Letting  $\bar{\eta}_s$  be the long-run average availability of the system,

$$\bar{\eta}_s = (ZBAR)^{15} = (.99792)^{15} \doteq \underline{\underline{.9693}}.$$

This compares with the average system availability over the first mission time of .9786.

(2) In this case  $ZBAR = .72414$  and  $\bar{\eta}_s \doteq \underline{\underline{.0079}}$ .

This compares with the average system availability over the first mission time of .076.

The above comparisons indicate the use of the long-run average availability to approximate the system availability over the first mission time is a conservative practice. These cases and others also indicate that the lower the value of  $ZBAR$  the more conservative is the practice.



# APPENDIX C

## FORTRAN IV COMPUTER PROGRAM FOR THE INVERSION OF $\eta^*(s)$ BY NUMERICAL METHODS

```

C   THIS PROGRAM COMPUTES VALUES OF SYSTEM AVAILABILITY BY
C   INVERTING THE LAPLACE TRANSFORM OF THE AVAILABILITY
C   FUNCTION.
C
C   IMPLICIT REAL*8(A-H),REAL*8(O-Z)
C   COMPLEX*16 S,ETA,EXPON,CONST,TOP,BOTTOM
C   DIMENSION XCOF(20),COF(20),ROOTR(20),ROOTI(20),S(20),
1  EXPON(20),RETA(20,7),YLAMDA(7),ZBAR(7),Z1(7),ETA(20)
C   DATA YLAMDA/0.005,0.010,0.05,0.1,0.2,0.3,0.4/
C   JCASF=0
C
C   ICASE IS THE NUMBER OF CASES TO BE PROCESSED THIS RUN.
C   READ(5,1) ICASE
1  FORMAT(I2)
5  READ(5,10) ALPHA,XMU,PZERO
10 FORMAT(F3.0,2F10.3)
C   JCASE=JCASF+1
C
C   WRITE(6,6) JCASE
6  FORMAT(1H1,45X,'CASE',I4)
DO 800 K=1,7
C   XLAMDA=YLAMDA(K)
C
C   WRITE(6,7)
7  FORMAT(/10X,'INPUT DATA')
C   WRITE(6,8) ALPHA, XMU, XLAMDA
8  FORMAT(/10X,'ALPHA = ',F3.0,5X,' MU = ',F10.3,5X,
1  'LAMBDA = ',F10.3)
C
C   PUT ZEROS IN ALL ARRAYS.
C   DO 80 L=1,20
C   XCOF(L)=0.0
C   COF(L)=0.0
C   ROOTR(L)=0.0
C   ROOTI(L)=0.0
C   S(L)=(0.0,0.0)
C   ETA(L)=(0.0,0.0)
80  EXPON(L)=(0.0,0.0)
C
C   M=ALPHA
C   N=M+1
C   IF(M.NE.ALPHA)GO TO 40
C
C   COMPUTE COEFFICIENTS OF THE POLYNOMIAL.
C   CALL COEFF(ALPHA,XMU,XLAMDA,XCOF)
C
C   FIND THE ROOTS OF THE POLYNOMIAL.
C   DPOLRT IS A PROGRAM LIBRARY SUBROUTINE.
C   CALL DPOLRT(XCOF,COF,N,ROOTR,ROOTI,IER)
C
C   60 WRITE(6,61) IER
C   IER IS AN ERROR CODE FROM SUBROUTINE DPOLRT.
61  FORMAT(/10X,'IER=',I2)
C   WRITE(6,18)
18  FORMAT(/13X,'ROOTS OF THE POLYNOMIAL. ')
C   WRITE(6,19)
19  FORMAT(/15X,'REAL',6X,'IMAGINARY' / )
14  WRITE(6,16) (ROOTR(I),ROOTI(I),I=1,N)
16  FORMAT(10X,2F12.5)
C
C   CHECK FOR MULTIPLE ROOTS.
C   CALL CKMULT(ROOTR,ROOTI,M)

```

```

C
C PUT THE ROOTS INTO THE COMPLEX ARRAY S(20).
DO 100 I=1,N
100 S(I)=DCMPLX(ROOTR(I),ROOTI(I))
C
C BEGIN INVERSION BY HEAVISIDE'S EXPANSION FORMULA.
C
DO 150 I=1,N
TOP=XMU+S(I)
BOTTOM=TOP+M*(XLAMDA+S(I))
CONST=TOP/BOTTOM
DO 150 J=1,20
EXPON(J)=CONST*DEXP(J*S(I)*0.05)
150 ETA(J)=ETA(J)+EXPON(J)
C
WRITE(6,160)
160 FORMAT(///10X,'VALUES OF THE AVAILABILITY FUNCTION AT'
1'.05 MISSION-TIME INCREMENTS.'/)
DO 170 I=1,20
T=0.05*I
170 WRITE(6,171)T,ETA(I)
171 FORMAT(10X,F4.2,2F10.6)
C
SUM=0.0
DO 155 L=1,20
RETA(L,K)=REAL(ETA(L))
155 SUM=SUM+RETA(L,K)
TOTSUM=SUM+SUM+1,-RETA(20,K)
C
C Z1 IS THE AVERAGE AVAILABILITY OVER THE FIRST MISSION-TIME
Z1(K)=TOTSUM/40.
C
C ZBAR IS THE LONG RUN TIME AVERAGE AVAILABILITY.
900 ZBAR(K)=XMU/(ALPHA*XLAMDA+XMU)
C
CALL OUTPUT(YLAMDA,ALPHA,PZERO,XMU,Z1,ZBAR,RETA)
C
30 IF(JCASE-ICASE)5,50,50
40 WRITE(6,41)
41 FORMAT(10X,'ERROR- ALPHA MUST BE AN INTEGER')
GO TO 30
50 STOP
END

SUBROUTINE CKMULT(ROOTR,ROOTI,M)
IMPLICIT REAL*8(A-H),REAL*8(O-Z)
DIMENSION S(1),ROOTR(1),ROOTI(1)
C
C THIS SUBROUTINE CHECKS FOR MULTIPLICITIES AMONG THE ROOTS
C
MULT=1
DO 50 I=1,M
K=M+1-I
DO 50 J=1,K
50 IF(ROOTR(I).EQ.ROOTR(I+J).AND.ROOTI(I).EQ.ROOTI(I+J))
1MULT=MULT+1
IF(MULT.NE.1) GO TO 60
C
WRITE(6,51)
51 FORMAT(///10X,'THERE ARE NO MULTIPLE ROOTS.')
```

```

RETURN
C
60 WRITE(6,61)
61 FORMAT(///10X,'THE POLYNOMIAL HAS MULTIPLE ROOTS. THIS
1PROGRAM WILL NOT ACCURATELY HANDLE THIS CASE.')
```

```

RETURN
END

```

```

SUBROUTINE COEFF(ALPHA,XMU,XLAMDA,XCOF)
IMPLICIT REAL*8(A-H),REAL*8(O-Z)
DIMENSION XCOF(1)

C
C THIS SUBROUTINE COMPUTES THE COEFFICIENTS OF THE EXPANDED
C POLYNOMIAL IN THE DENOMINATOR OF THE LAPLACE TRANSFORM.
C
M=ALPHA
N2=M+2
X=ALPHA+1.0
XCOF(1)=0.0
XCOF(M+2)=1.0
CHOOZ=M
DO 20 I=1,M
BKT=XLAMDA+(XMU*I)/(X-I)
XCOF(I+1)=CHOOZ*BKT*XMU***(M-I)
20 CHOOZ=CHOOZ*(M-I)/(I+1)

C
C THE COEFFICIENTS ARE NOW IN THE ARRAY,XCOF.
C
WRITE(6,17)
17 FORMAT(/10X,'COEFFICIENTS OF THE POLYNOMIAL')
WRITE(6,12)(XCOF(I),I=1,N2)
12 FORMAT(/10X,10F12.6)
RETURN
END

SUBROUTINE OUTPUT(YLAMDA,ALPHA,PZERO,XMU,Z1,ZBAR,RETA)
IMPLICIT REAL*8(A-H),REAL*8(O-Z)
DIMENSION YLAMDA(1),Z1(1),ZBAR(1),RETA(20,7)
WRITE(6,1)ALPHA,PZERO,XMU
1 FORMAT(1H1,/////////25X,'ALPHA=',F4.1,5X,'PZERO=',F5.2,
15X,'MU=',F5.2)
WRITE(6,11)
11 FORMAT(/46X,'LAMBDA')
WRITE(6,2)(YLAMDA(L),L=1,7)
2 FORMAT(/22X,F4.3,6(4X,F4.3))
WRITE(6,12)
12 FORMAT(15X,'TIME'/)
DO 50 I=1,20
T=0.05*I
50 WRITE(6,3)T,(RETA(I,J),J=1,7)
3 FORMAT(15X,F4.2,7(2X,F6.5)/)

C
WRITE(6,4)(Z1(I),I=1,7)
4 FORMAT(/16X,'Z1',1X,7(2X,F6.5)/)
WRITE(6,5)(ZBAR(I),I=1,7)
5 FORMAT(15X,'ZBAR',7(2X,F6.5))
RETURN
END

```

## BIBLIOGRAPHY

1. Cox, D. R., Renewal Theory, p. 80-84, Methuen & Co. Ltd, 1962.
2. Hosford, J. E., "Measures of Dependability," Operations Research, v.8, p. 53-64, 1960.
3. Jacobson, H. I., "An Interval Estimate of System Availability," Operations Research, v. 14, p. 460-465, 1966.
4. Spiegel, M. R., Theory and Problems of Laplace Transforms, p. 61, Schaum, 1965.
5. Statistical Theory of Reliability, edited by Marvin Zelen [and others], The University of Wisconsin Press, 1963.

# INITIAL DISTRIBUTION LIST

	No. Copies
1. Defense Documentation Center Cameron Station Alexandria, Virginia 22314	20
2. Library, Code 0212 Naval Postgraduate School Monterey, California 93940	2
3. Civil Schools Branch Office of Personnel Operations Washington, D.C. 20315	1
4. Department of Operations Analysis, Code 55 Naval Postgraduate School Monterey, California 93940	1
5. Associate Professor W. M. Woods, Code 55 Naval Postgraduate School Monterey, California 93940	4
6. Major George R. Catron, USA 1050 Madrid Court Seaside, California 93955	1
7. Commanding General U.S. Army Transportation School Fort Eustis, Virginia 23604	1
8. Commanding General U.S. Army Materiel Command Washington, D.C. 20315	1



UNCLASSIFIED

Security Classification

## DOCUMENT CONTROL DATA - R &amp; D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1. ORIGINATING ACTIVITY (Corporate author) Naval Postgraduate School Monterey, California 93940		2a. REPORT SECURITY CLASSIFICATION Unclassified	
		2b. GROUP	
3. REPORT TITLE INVESTIGATION OF THE ACCURACY OF USING STEADY-STATE RESULTS TO APPROXIMATE ACTUAL SYSTEM AVAILABILITY			
4. DESCRIPTIVE NOTES (Type of report and, inclusive dates) Master's thesis; April 1970			
5. AUTHOR(S) (First name, middle initial, last name) George Richard Catron, Major, United States Army			
6. REPORT DATE April, 1970		7a. TOTAL NO. OF PAGES 41	7b. NO. OF REFS 5
8a. CONTRACT OR GRANT NO.		9a. ORIGINATOR'S REPORT NUMBER(S)	
b. PROJECT NO.			
c.		9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report)	
d.			
10. DISTRIBUTION STATEMENT This document has been approved for public release and sale; its distribution is unlimited.			
11. SUPPLEMENTARY NOTES		12. SPONSORING MILITARY ACTIVITY Naval Postgraduate School Monterey, California 93940	
13. ABSTRACT  Values of system availability are computed for a system whose failure density is exponential ( $\lambda$ ) and whose repair density is special Erlang ( $\mu, \alpha$ ). The system is modeled as an alternating renewal process. The Laplace transform of the availability function is developed and inverted (by using a numerical procedure) to obtain the values of the system availability. Corresponding values of the long-run average system availability and the average availability over the first mission time are also computed. Comparisons are made which establish that using the long-run average value to approximate the true availability over the first mission time is a conservative practice.			

14

### KEY WORDS

LINK A

LINK B

LINK C

ROLE

WT

NAME	ROLE
Mr. J. Edgar Hoover	Director
Mr. Clegg	Chief of Bureau
Mr. Glavin	Chief of Bureau
Mr. Ladd	Chief of Bureau
Mr. Nichols	Chief of Bureau
Mr. Rosen	Chief of Bureau
Mr. Tracy	Chief of Bureau
Mr. Carson	Chief of Bureau
Mr. Egan	Chief of Bureau
Mr. Gurnea	Chief of Bureau
Mr. Hendon	Chief of Bureau
Mr. Pennington	Chief of Bureau
Mr. Quinn	Chief of Bureau
Mr. Nease	Chief of Bureau
Mr. Gandy	Chief of Bureau

WT

ROLE

WT

## INVERSE LAPLACE TRANSFORM











Thesis  
C333

Catron

118435

c.1

Investigation of  
the accuracy of using  
steady-state results  
to approximate actual  
system availability.

Thesis  
C333

Catron

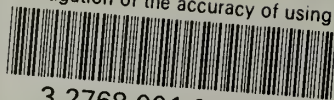
118435

c.1

Investigation of  
the accuracy of using  
steady-state results  
to approximate actual  
system availability.

thesC333

Investigation of the accuracy of using s



3 2768 001 02178 5

DUDLEY KNOX LIBRARY